## Layout Power Supply Boards to Minimize EMI - Part 3: EMI Basics

PC-board layout sets the functional, electromagnetic interference (EMI), and thermal behavior of a power supply. Good layout from first prototyping on actually saves significant resources in EMI filters, mechanical shielding, EMI test time, and PC board runs. This segment reviews some of the basic fundamentals of EMI and EMC.

electromagnetic far field impedance is about  $377\Omega = 120\pi$  or  $29,9792458 \times 4 \times \pi\Omega$  for the vacuum velocity of light. Any electromagnetic wave far enough from its source (rule of thumb >wavelength/2  $\times$   $\pi$ ) has a 377 $\Omega$  relationship between its magnetic and electric field. Closer to the source, it can be a perfectly matched antenna, which transforms its input power source to the right  $377\Omega$  electromagnetic field. Or, there is significant mismatch and the antenna starts mainly as a magnetic field source or an electric field

source.

The magnetic field source has a lower impedance of  $377\Omega$ . The electric field source has a higher than  $377\Omega$  impedance. The graph in Fig. 23 shows that, regardless if it starts as an electric or a magnetic field source, the electromagnetic field balances itself to its far field impedance at a distance of:

$$\frac{\lambda}{2\pi}$$
 (1)

where  $\lambda = \text{Wavelength}$ 

Nonisolated switch mode power supply units have primarily magnetic field sources, since the impedances of the EMI-relevant loops with high di/dt are much lower than  $377\Omega$  unless you have very low current high voltage power supplies. So minimizing the AC magnetic fields on any nonisolated power supply unit will be the key to success.

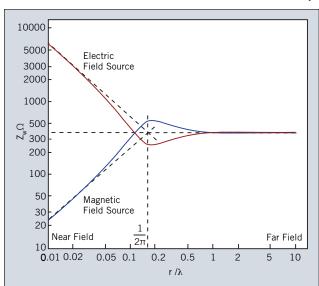


Fig. 23. Regardless if it starts as an electric or a magnetic field source, the electromagnetic field balances itself to its far field impedance.

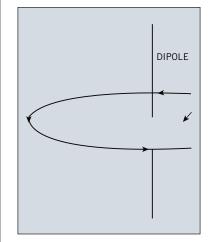


Fig. 24. The AC current flows around an area and creates the magnetic field part of a normal dipole antenna.

Any isolated power supply unit will have AC loops with lower than 377  $\Omega$ , where the same magnetic field minimization as on nonisolated PSUs will be required. However, due to the very nature of isolation, we need higher impedances between the isolation barrier. On the isolation barrier, which is mostly done with a transformer, we try to get  $M\Omega$  of isolation. On the isolation barrier, the electric AC field dominates and requires a different strategy. Here we try to get as low capacitive field coupling as possible. So we try to get as much distance as possible and to minimize the size of any conductive material.

## DIPOLE ANTENNA EFFECT OF THE HOT LOOP

When analyzing what the hot loop does, magnetic dipole antennas give a good clue.

The AC current flows around an area and creates the magnetic field part of a normal dipole antenna, as shown in *Fig. 24*).

Magnetic antennas with loop diameters << $\lambda$  have very low radiation resistance. The range:  $\mu\Omega$  to  $m\Omega$ .

$$R_R = 320\pi^4 \left[ \frac{NF}{\lambda^2} \right]^2 (2)$$

 $R_R$  = Radiation resistance in ohms F = Area of magnetic loop

N = Number of turns (= 1 in most layouts)

 $\lambda = Wavelength$ 

with 
$$\lambda = \frac{c}{f}$$
 and  $N = 1$  for all

practical layout loops

$$R_{R} = \frac{320\pi^{4} f^{4} F^{2}}{c^{4}} \quad (3)$$

 $c = Speed of light \approx 300000 km/s$ f = Frequency

The radiation resistance is low  $(m\Omega)$  for typical dimensions of a PC-board power supply unit. Increasing the radiation resistance improves the matching and increases emitted radiation proportional to

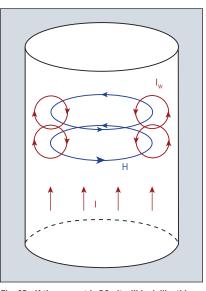


Fig. 25. If the current is DC, it will look like this. Because I is constant, the resulting H is constant and  $I_{\rm w}$  is zero. In a case that I has an AC content, which means there is di/dt, then the resulting magnetic field H changes.

the radiation resistance. The parameter we can influence the most with layout is the area of the magnetic loop. The emitted radiation is proportional to the square of this area.

## SKIN EFFECT

To understand the effect of shielding, we need to dig a bit into the electromagnetic properties of the materials used. Electric cur-

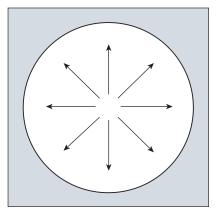


Fig. 26. Forces that move the current density to the outside of a conductor are called skin effect.

rent, whether or not it is tied to a conductor, will always flow on the path of least impedance. For higher frequencies, this will be the path of least inductance. This means the current will also flow on the path of its lowest losses. Electric conduction material minimizes any internal magnetic AC fields by creating eddy currents that oppose AC fields internal to the conducting material. Viewed from the outside, this looks like the skin effect, because the current density is forced to the outside of the conductor.

For another example, assume that the current, I, flows uniformly through a cylinder. This is a typical case for DC current.

If the current is DC, then it will look like the shape in Fig. 25. I is a

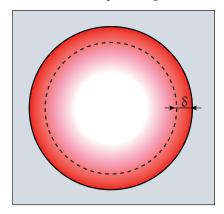


Fig. 27. Wall thickness of a pipe, which would give the same resistance at DC as a full cylinder wire at AC, is called skin depth.

constant, so the resulting H is constant and  $I_W$  is zero. In the case that I has an AC content, which means there is di/dt, then the resulting magnetic field H changes. The changing magnetic field H creates induction voltage and since we are inside a conductor, the induction voltage creates an induced current  $I_W$ , often referred to as eddy current. Eddy currents will create losses. If we assume that nature minimizes these losses, the only way to minimize this is to change the original uniform current distribution and let all current flow only at the surface of the cylinder. Now the magnetic field H is only at the surface of the cylinder. This way, the eddy currents  $I_W$  are moved to the outside and the return path is cut off, omitting most of the eddy currents and its losses.

## SKIN EFFECT AND SKIN DEPTH

We can think of forces (*Fig. 26*) that move the current density to the outside of a conductor. This is called skin effect. The wall thickness of a pipe, which would give the same resistance at DC as a full cylinder wire at AC, is called skin depth (*Fig. 27*). Since the forces moving the current density to the outside are a result of the induc-

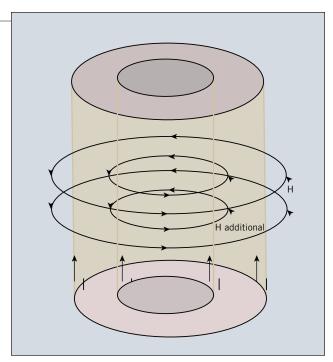
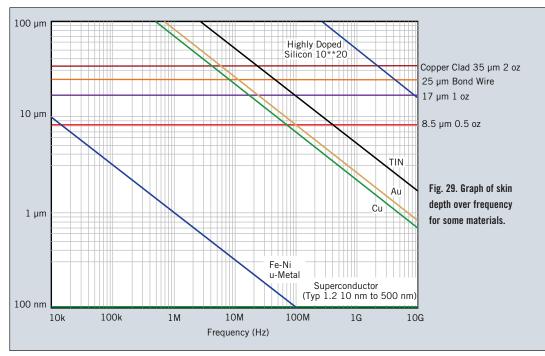


Fig. 28. Large diameter pipe wall conducting all the current on its surface. Total inductance of a given length of this wire is the complete volume integral of its magnetic field up to infinity or whatever physical size you assume for the universe.

tion law, the skin depth goes down with rising frequency. Skin depth goes down with rising conductivity and goes down with increasing magnetic permeability.

For another example, assume we have a pipe wall conducting all the current on its surface, as shown in the large diameter in Fig. 28. Total inductance of a given length of this wire (1 meter or 1 foot whatever is most suitable) is the complete volume integral of its magnetic field up to infinity or



whatever physical size you assume for the universe.

Now we shrink the pipe diameter to the smaller inner one shown in Fig. 28. The magnetic field is still the same as the larger pipe to infinity. However, we now have an additional magnetic field volume between the new small pipe and the prior larger pipe diameter. So the total integral of the magnetic field is now larger. This shows that the inductance is larger for a thinner conductor of a given length. Or, we can assume that the inductance

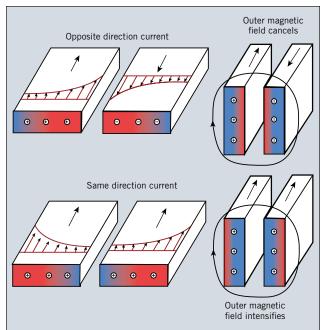


Fig. 30. Opposite direction current forces will attract the currents to each other, which is called proximity effect.

increases as more of the current moves from the outer wall to the center of the wire. If we apply a voltage over both ends of the wire, the resulting current distribution is determined by the impedance. Since the inductance in the center is higher, most current density moves to the surface. The most extreme case of skin effect in conductors with zero resistance is shown in superconductors. There, quantum effects prevent all current from being bound to an outer layer of zero thickness. The thickness where most current is concentrated on superconductors is called London depth.

A graph of skin depth over frequency for some materials is shown in Fig. 29. We see that copper on typical PC-board material is affected by skin effect in the range of 5 MHz to 50 MHz. And, we see that even highly doped silicon at the thickness typically used on ICs is only affected in the terahertz region. Copper (Cu) and gold (Au) are close together. Materials with high magnetic permeability, such as Fe-Ni, have low skin depth, even at audio frequencies. For this reason, material with high magnetic permeability is used to shield audio transformers.

AC current through a good conductor will push current density to the outside. The current will flow where the impedance, dominated by inductance, is lowest. With regard to the impact of skin effect on layout and components, we can derive simple guidelines. Better is short and thick or wide. Reverse geometry capacitors have lower ESL because they are shorter and thicker. If we have opposite direction current, the same forces will attract the currents to each other (Fig. 30). This is called proximity effect. **U**